mation to the collision term is

A. The Boltzmann Equation. The Boltzmann equation in the relaxation time approxi-

$$\frac{\partial f}{\partial t} + \mathbf{v} \cdot \nabla_{\mathbf{x}} f + \mathbf{F} \cdot \nabla_{\mathbf{p}} f = -\frac{f - f_0}{\tau},\tag{1}$$

where  $f = f(\mathbf{x}, \mathbf{p}, t)$  is the density of particles at  $(\mathbf{x}, \mathbf{p})$  at time t and

- 1.  $f_0 = f_0(\mathbf{x}, \mathbf{p})$  is the equilibrium distribution function at  $(\mathbf{x}, \mathbf{p})$ ,
- 2.  $\nabla_{\mathbf{x}} = \partial/\partial \mathbf{x}$  and  $\nabla_{\mathbf{p}} = \partial/\partial \mathbf{p}$ ,
- 3.  $\tau$  is the relaxation time, a characteristic time for departures from equilibrium to return to equilibrium.

This equation is space-time local, i.e., the equilibrium distribution function can vary from place to place, can vary *slowly* in time. The variations in space are on a scale large compared to the mean free path, the variations in time are slow compared to  $\tau$ .

The proper venue for deriving the Boltzmann equation from a more fundamental description is non-equilibrium statistical physics, where one starts with the Liouville equation for the density in classical phase space. If you are interested http://denali.phys.uniroma1.it/ puglisi/thesis/node20.html.

**B.** Uses for  $f(\mathbf{x}, \mathbf{p}, t)$ .

1. Calculate local averages

$$\langle A(t) \rangle = \frac{\int d\mathbf{x} \int d\mathbf{p} \ A(\mathbf{x}, \mathbf{p}) f(\mathbf{x}, \mathbf{p}, t)}{\int d\mathbf{x} \int d\mathbf{p} \ f(\mathbf{x}, \mathbf{p}, t)}.$$
(2)

2. Find an equation of motion for the average of A, e.g.,

$$\frac{\partial \langle A \rangle}{\partial t} + \cdots, \tag{3}$$

see below.

)

## C. Examples of $f_0(\mathbf{x}, \mathbf{p})$ .

1. ideal gas of N particles, in a uniform space of volume V, in contact with a temperature reservoir at T:

$$f_0(\mathbf{x}, \mathbf{p}) = \frac{N}{V} I_0^{-3} exp\left(-\beta \frac{\mathbf{p}^2}{2m}\right), \qquad (4)$$

$$n(\mathbf{x}) = \int d\mathbf{p} \ f_0(\mathbf{x}, \mathbf{p}) = \frac{N}{V}, \tag{5}$$

$$1 = \int d\mathbf{p} \ I_0^{-3} exp\left(-\beta \frac{\mathbf{p}^2}{2m}\right). \tag{6}$$

2. ideal gas of N particles, each particle confined by the single particle potential  $U(\mathbf{x})$ , in contact with a temperature reservoir at T:

$$f_0(\mathbf{x}, \mathbf{p}) = N I_U^{-1} I_0^{-3} exp\left(-\beta \left[\frac{\mathbf{p}^2}{2m} + U(\mathbf{x})\right]\right), \tag{7}$$

$$n(\mathbf{x}) = \int d\mathbf{p} \ f_0(\mathbf{x}, \mathbf{p}) = N I_U^{-1} exp\left(-\beta U(\mathbf{x})\right), \tag{8}$$

$$1 = \int d\mathbf{p} \ I_0^{-3} exp\left(-\beta \frac{\mathbf{p}^2}{2m}\right),\tag{9}$$

$$1 = \int d\mathbf{x} \ I_U^{-1} exp\left(-\beta U(\mathbf{x})\right). \tag{10}$$

3. ideal gas of N particles, with average x-momentum P, in a uniform space of volume V, in contact with a temperature reservoir at T:

(a)

$$f_0(\mathbf{x}, \mathbf{p}) = \frac{N}{V} I_0^{-2} I_Q^{-1} exp\left(-\beta \left[\frac{\mathbf{p}^2}{2m} - Qp_x\right]\right), \qquad (11)$$

$$n(\mathbf{x}) = \int d\mathbf{p} \ f_0(\mathbf{x}, \mathbf{p}) = \frac{N}{V}, \tag{12}$$

$$1 = \int d\mathbf{p} \ I_0^{-2} I_Q^{-1} exp\left(-\beta \left[\frac{\mathbf{p}^2}{2m} - Qp_x\right]\right). \tag{13}$$

(b)

$$P = \langle p_x \rangle = \frac{1}{\beta} \frac{d}{dQ} ln I_Q, \tag{14}$$

$$I_Q = \int dp \, exp\left(-\beta \left[\frac{p^2}{2m} - Qp\right]\right). \tag{15}$$

(c) the symmetry  $\mathbf{p} \to -\mathbf{p}$  is broken by the Q term, consequently  $\langle p_x \rangle$  is non-zero. How is Q related to  $\langle p_x \rangle = P$ ?

## **D.** An equation of motion for $\langle A \rangle$ . Define

$$n = n(\mathbf{x}, t) = \int d\mathbf{p} \ f(\mathbf{x}, \mathbf{p}, t), \tag{16}$$

$$\langle A \rangle = \langle A(\mathbf{x},t) \rangle = \frac{\int d\mathbf{p} A f(\mathbf{x},\mathbf{p},t)}{\int d\mathbf{p} f(\mathbf{x},\mathbf{p},t)}.$$
 (17)

Note. In this section  $<\cdots>$  is an average over  ${\bf p}$  only!!!

For A independent of t multiply Eq. (1) by A and integrate on  $\mathbf{p}$ :

1. first term in Eq. (1)

$$\int d\mathbf{p} \ A \ \frac{\partial f}{\partial t} = \frac{\partial \ (n < A >)}{\partial t} = \frac{\partial < nA >}{\partial t}.$$
(18)

2. second term in Eq. (1)

$$\int d\mathbf{p} \ A \ (\mathbf{v} \cdot \nabla_{\mathbf{x}}) \ f = \nabla_{\mathbf{x}} \cdot \langle nA\mathbf{v} \rangle - \langle n\mathbf{v} \cdot \nabla_{\mathbf{x}}A \rangle, \tag{19}$$

[use  $\nabla \cdot (A\mathbf{v}f) = f \mathbf{v} \cdot \nabla A + A \mathbf{v} \cdot \nabla f$ ].

3. third term in Eq. (1)

$$\int d\mathbf{p} \ A \ (\mathbf{F} \cdot \nabla_{\mathbf{p}}) \ f = \int d\mathbf{p} \ \nabla_{\mathbf{p}} \cdot (A\mathbf{F}f) - \int d\mathbf{p} \ Af\nabla_{\mathbf{p}} \cdot \mathbf{F}) - \langle n\mathbf{F} \cdot \nabla_{\mathbf{p}}A \rangle,$$
(20)  
= - < n\mathbf{F} \cdot \nabla\_{\mathbf{p}}A >, (21)

where the simplification occurs because the first integral goes to a surface in **p**-space that can be arbitrarily far away (where f = 0) and we assume the applied forces are independent of **p** (re-think this if velocity dependent forces are involved).

4. assume that A is a quantity that is conserved by the collision process so that the term on the RHS of Eq. (1) is dropped.

Assemble the pieces

$$\frac{\partial \langle nA \rangle}{\partial t} + \nabla_{\mathbf{x}} \langle nA\mathbf{v} \rangle - \langle n\mathbf{v} \cdot \nabla_{\mathbf{x}}A \rangle - \langle n\mathbf{F} \cdot \nabla_{\mathbf{p}}A \rangle = 0, \tag{22}$$

$$\frac{\partial \langle nA \rangle}{\partial t} + \nabla_{\mathbf{x}} \langle nA\mathbf{v} \rangle - n \langle \mathbf{v} \cdot \nabla_{\mathbf{x}}A \rangle - n \mathbf{F} \langle \nabla_{\mathbf{p}}A \rangle = 0,$$
(23)

where the second line is a possibly convenient re-arrangement. The quantity  $\langle nA \rangle$  is a density and  $\langle nA\mathbf{v} \rangle$  the corresponding current.

- E. Conservation laws. Make 5 choices for  $A, A = m, mv_i$  (i = x, y, z), kinetic energy.
  - 1.  $A = m, \rho = mn, \mathbf{J}_{\rho} = \langle \rho \mathbf{v} \rangle = \rho \langle \mathbf{v} \rangle = \rho \mathbf{u},$  $\frac{\partial \rho}{\partial t} + \nabla \cdot \mathbf{J}_{\rho} = 0.$  (24)
  - 2.  $A = mv_i$ ,

$$\frac{\partial < \rho v_i >}{\partial t} + \sum_k \frac{\partial < \rho v_i v_k >}{\partial x_k} = \frac{1}{m} \rho F_i.$$
(25)

**massage**. Use  $\langle \rho v_i \rangle = \rho u_i$  and

$$v_i v_k = (v_i - u_i)(v_k - u_k) + v_i u_k + v_k u_i - u_i u_k, \qquad (26)$$

$$<\rho v_i v_k> = \rho < v_i v_k> = \rho < (v_i - u_i)(v_k - u_k) > +\rho u_i u_k,$$
(27)

to write

$$\frac{(\partial\rho u_i)}{\partial t} + \sum_k \frac{\partial(\rho u_i u_k)}{\partial x_k} = \frac{1}{m} \rho F_i - \sum_k \frac{\partial}{\partial x_k} \rho < (v_i - u_i)(v_k - u_k) > .$$
(28)

Define the pressure tensor

$$P_{ik} = \rho < (v_i - u_i)(v_k - u_k) >$$
(29)

and find

$$\frac{\partial u_i}{\partial t} + \mathbf{u} \cdot \nabla u_i = \frac{1}{m} F_i - \sum_k \frac{1}{\rho} \frac{\partial P_{ik}}{\partial x_k}.$$
(30)

[To get here from Eq. (27) we used Eq. (23) to get rid of the derivatives of  $\rho$ .]

3.  $A = m|\mathbf{v} - \mathbf{u}|^2/2$ , this is the kinetic energy in the motion of the particles in the gas relative to the local average velocity, an energy that will be identified with the temperature.

$$\frac{1}{2}\frac{\partial}{\partial t} < \rho |\mathbf{v} - \mathbf{u}|^2 > + \frac{1}{2}\sum_k \frac{\partial}{\partial x_k} < \rho v_k |\mathbf{v} - \mathbf{u}|^2 > -\frac{1}{2}\rho \sum_k < v_k \frac{\partial}{\partial x_k} |\mathbf{v} - \mathbf{u}|^2 > = 0.$$
(31)

**massage**. Define (think  $E = (3/2)k_BT$ ,  $\theta \leftrightarrow k_BT$ )

$$\theta = \frac{1}{3}m < |\mathbf{v} - \mathbf{u}|^2 >, \tag{32}$$

$$\mathbf{Q} = \frac{1}{2}\rho < (\mathbf{v} - \mathbf{u}) |\mathbf{v} - \mathbf{u}|^2 > .$$
(33)

Then

$$\frac{1}{2}\rho < v_i \ |\mathbf{v} - \mathbf{u}|^2 > = \frac{1}{2}\rho < (v_i - u_i) \ |\mathbf{v} - \mathbf{u}|^2 > +\frac{1}{2}\rho u_i < |\mathbf{v} - \mathbf{u}|^2 >, \quad (34)$$

$$= Q_i + \frac{3}{2}(\rho \ \theta \ u_i) \quad \rightarrow \quad conduct + convect, \tag{35}$$

and using  $\rho < v_k \partial (|\mathbf{v} - \mathbf{u}|^2) / \partial x_k > = -\rho < v_k \sum_i (v_i - u_i) > \partial u_i / \partial x_k$  and

$$\rho < v_k \ (v_i - u_i) > = \ \rho < (v_k - u_k)(v_i - u_i) > +\rho u_k < v_i - u_i >, \tag{36}$$

$$= P_{ki}, (37)$$

find

$$\frac{3}{2}\frac{\partial}{\partial t}(\rho \ \theta) + \frac{3}{2}\nabla \cdot (\rho \ \theta \ \mathbf{u}) + \nabla \cdot \mathbf{Q} + m\sum_{k}\sum_{i}P_{ki}\frac{\partial u_{i}}{\partial x_{k}} = 0.$$
(38)

A final definition

$$M_{ik} = \frac{m}{2} \left( \frac{\partial u_i}{\partial x_k} + \frac{\partial u_k}{\partial x_i} \right), \tag{39}$$

use of Eq. (23) again and we have

$$\rho\left(\frac{\partial}{\partial t} + \mathbf{u} \cdot \nabla\right)\theta = -\frac{2}{3}\nabla \cdot \mathbf{Q} - \frac{2}{3}\sum_{k}\sum_{i}P_{kj}M_{jk} = 0.$$
(40)

## F. Collect and Interpret.

$$\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \mathbf{u}) = 0. \tag{41}$$

$$\left(\frac{\partial}{\partial t} + \mathbf{u} \cdot \nabla\right) u_i = \frac{1}{m} F_i - \sum_k \frac{1}{\rho} \frac{\partial P_{ik}}{\partial x_k},\tag{42}$$

$$= external force + internal force.$$
(43)

$$\rho\left(\frac{\partial}{\partial t} + \mathbf{u} \cdot \nabla\right)\theta = -\frac{2}{3}\nabla \cdot \mathbf{Q} - \frac{2}{3}\sum_{k}\sum_{i}P_{kj}M_{jk} = 0, \qquad (44)$$

$$= conduction + internal work.$$
(45)

Definitions:

$$n(\mathbf{x},t) = \int d\mathbf{p} \ f(\mathbf{x},\mathbf{p},t), \tag{46}$$

$$\langle \cdots (\mathbf{x}, t) \rangle = \frac{1}{n} \int d\mathbf{p} \cdots f(\mathbf{x}, \mathbf{p}, t),$$
 (47)

$$\rho(\mathbf{x},t) = mn, \tag{48}$$

$$\mathbf{u}(\mathbf{x},t) = \langle \mathbf{v} \rangle,\tag{49}$$

$$\theta(\mathbf{x},t) = \frac{1}{3}m < |\mathbf{v} - \mathbf{u}|^2 >, \tag{50}$$

$$\mathbf{Q}(\mathbf{x},t) = \frac{1}{2}\rho < (\mathbf{v} - \mathbf{u})|\mathbf{v} - \mathbf{u}|^2 >,$$
(51)

$$P_{ij}(\mathbf{x},t) = \rho < (v_i - u_i)(v_j - u_j) >, \tag{52}$$

$$M_{ik}(\mathbf{x},t) = \frac{m}{2} \left( \frac{\partial u_i}{\partial x_k} + \frac{\partial u_k}{\partial x_i} \right).$$
(53)