

Viscous Fluid Flow.

1. The equations. We will deal with a viscous fluid in the case that the density is constant. Then the equations for mass conservation and momentum conservation reduce to

$$\nabla \cdot \mathbf{v} = 0, \quad (1)$$

$$\frac{\partial \mathbf{v}}{\partial t} + (\mathbf{v} \cdot \nabla) \mathbf{v} = -\frac{1}{\rho_0} \nabla P + D_\eta \nabla^2 \mathbf{v}, \quad (2)$$

where $D_\eta = \eta/\rho_0$ is the viscous diffusion constant. See the Table on LL 46 for some numbers.

2. The stress tensor and R_e . Two formal statements about Eqs. (1) and (2).

1. The forces on the RHS of Eq. (2) can be formally arranged to define a stress tensor

$$\frac{\partial v_i}{\partial t} + (\mathbf{v} \cdot \nabla) v_i = -\frac{1}{\rho_0} \frac{\partial P}{\partial x_i} + D_\eta \nabla^2 v_i = \frac{1}{\rho_0} \sum_j \frac{\partial \sigma_{ij}}{\partial x_j}, \quad (3)$$

$$\sigma_{ij} = -P \delta_{ij} + \eta \left(\frac{\partial v_i}{\partial x_j} + \frac{\partial v_j}{\partial x_i} \right), \quad (4)$$

where the viscosity term has been symmetrized (check to see that this procedure leads to no change in the Navier-Stokes equation, Eq. (2)).

2. The size of the inertial term $(\mathbf{v} \cdot \nabla) v_i$ and the viscous stress term are

(a) inertial $(\mathbf{v} \cdot \nabla) v_i \sim U^2/L$,

(b) viscous stress $D_\eta \nabla^2 v_i \sim D_\eta U/L^2$.

The ratio, defined to be the **Reynolds number**, is

$$R_e = \frac{UL}{D_\eta} = \frac{L^2/D_\eta}{L/U} = \frac{\tau_D}{\tau_U}. \quad (5)$$

Here τ_D is the time to diffuse the distance L and τ_U is the time to travel that distance at velocity U . When $R_e \ll 1$ diffusion over L is much faster than fluid flow. In the opposite limit, $R_e \gg 1$ the diffusion and viscosity are relatively unimportant.

<http://www.aip.org/pt/jan00/berg.htm>. Life at $R_e = 10^{-4}$.

E. coli, a self-replicating object only a thousandth of a millimeter in size, can swim

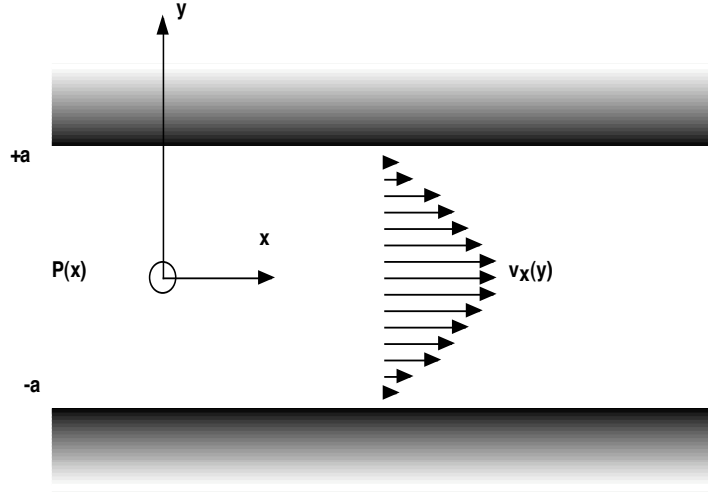


FIG. 1: Poiseuille Flow.

35 diameters a second, taste simple chemicals in its environment, and decide whether life is getting better or worse.

– Howard C. Berg

<http://socrates.berkeley.edu/~shaevitz/Movies/Spiroplasma%20Kinking.mov>

3. Viscosity at work; two examples.

3a. Poiseuille Flow

Consider a fluid between two parallel plates, separated by $2a$, that flows in response to a steady pressure gradient. See Fig. 1. Since $\mathbf{v} = (v_x(y), 0, 0)$ the $(\mathbf{v} \cdot \nabla)v_x$ term in Eq. (2) is zero and we have

$$-\frac{1}{\rho_0} \frac{\partial P}{\partial x} + D_\eta \frac{\partial^2 v_x}{\partial y^2} = 0. \quad (6)$$

For a non slip boundary condition at $y = \pm a$ we have

$$\rho_0 v_x(y) = \frac{1}{2} \frac{a^2}{D_\eta} \left| \frac{\partial P}{\partial x} \right| \left(1 - \frac{y^2}{a^2} \right) = \frac{1}{2} \tau_\eta \left| \frac{\partial P}{\partial x} \right| \left(1 - \frac{y^2}{a^2} \right), \quad (7)$$

a parabolic velocity profile for which the maximum velocity, at $y = 0$, is proportional to $\tau_\eta = a^2/D_\eta$. This fluid flow, called Poiseuille flow, is controlled by the rate at which the viscosity carries momentum, delivered to the fluid by the pressure gradient, to the walls of

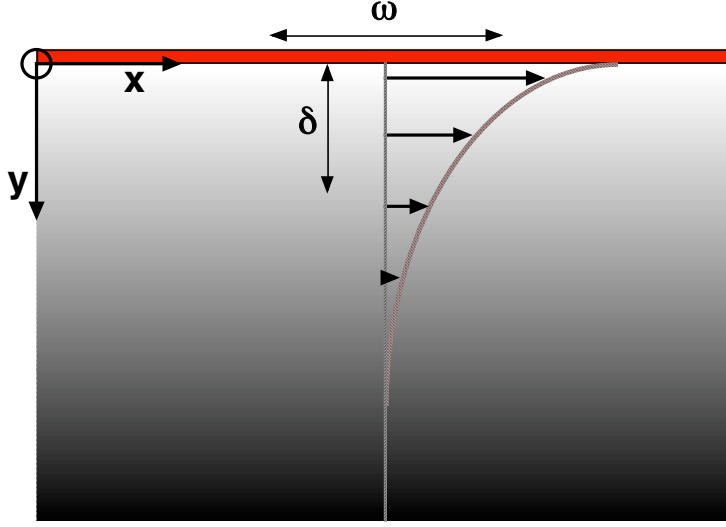


FIG. 2: Viscous penetration depth.

the flow space where it is lost. Hence the involvement of τ_η .

1. The total flow of fluid $Q = \int \rho_0 v_x(y) dy \propto a^3$.
2. For a circular pipe expect $Q \propto a^4$, LL (17.10).
3. For a current in a conductor $I = V/R$ and $R = \rho L/A$ (here ρ is the resistivity, L the length of the conductor and $A \propto a^2$ the cross sectional area). Thus $I \propto a^2$

3b. Viscous penetration depth.

See Fig. 2. Suppose the upper surface of a fluid is in contact with a solid surface that is oscillated at frequency ω . The fluid "sticks" to the surface so the upper edge of the fluid moves with velocity $v_x(y=0) = A \exp(-i\omega t)$. The equation of motion for the fluid is

$$\frac{\partial v_x}{\partial t} = D_\eta \frac{\partial^2 v_x}{\partial y^2}, \quad (8)$$

the x-component of Eq. (2), P does not depend on x and the inertial term is zero because v_x depends only on y . For $v_x(y) = U(y) \exp(-i\omega t)$ find

$$\frac{\partial^2 U}{\partial y^2} = (-i\omega/D_\eta)U = -\kappa^2 U, \quad (9)$$

and

$$U(y) = A \exp(iky) = A \exp(ik_1y) \exp(-k_1y) = A \exp(ik_1y) \exp(-y/\delta_\eta) \quad (10)$$

where $k_1^2 = \omega/2D_\eta$ and δ_η is the viscous penetration depth. The disturbance at the surface at frequency ω penetrates into the interior of the liquid to the approximate depth to which momentum can diffuse on time scale $T_\omega \approx \omega^{-1}$, $D_\eta T_\omega \approx \delta_\eta^2$.

The physics here is similar to that associated with the skin depth in E and M. In that case an electric field on the surface of a conductor attempts to move the electron gas within the conductor at frequency ω . It succeeds to depth

$$\delta_\sigma^2 \approx \frac{c^2/\sigma}{\omega} \approx D_\sigma T_\omega, \quad (11)$$

where $c^2/\sigma = D_\sigma$, σ is the conductivity. Jackson, Sec. 7.7.

4. Low Reynolds number flow, the Stokes problem.

The problem is that of a sphere, radius R , moving through a viscous fluid with velocity $\mathbf{u} = (0, 0, u)$. The problem solved is that of a sphere at rest with a fluid, having velocity \mathbf{u} at large distance, moving past the sphere. This is a steady flow problem; the equations to be solved are

$$\nabla \cdot \mathbf{v} = 0, \quad -\nabla P + \eta \nabla^2 \mathbf{v} = 0. \quad (12)$$

This is an algebra intensive problem. Begin by removing the pressure from the problem (we can come back and *learn it* at the end. [Here the pressure is an output, not an input.] Take **curl** of the second of Eq. (12) and use $\nabla \cdot \mathbf{u} = 0$ to find the two equations of interest

$$\nabla \cdot (\mathbf{v} - \mathbf{u}) = 0, \quad \nabla^2 \nabla \times \mathbf{v} = 0. \quad (13)$$

From first of these suggests writing $\mathbf{v} - \mathbf{u}$ as the **curl** of a vector field so that $\nabla \cdot$ will be automatically satisfied. Then, it is from the second that the conditions on this potential are established.

$$\mathbf{v} - \mathbf{u} = \nabla \times \mathbf{A}. \quad (14)$$

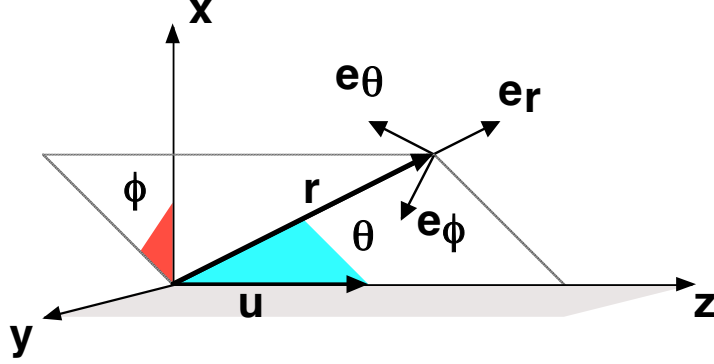


FIG. 3: Coordinate system.

The velocity field has **no** components in the \mathbf{e}_ϕ direction, by symmetry, Fig. 3. Look in Griffiths or Jackson; the vector potential points in that direction so that there are non-zero e_r and e_θ components. So the vector potential can be written in the form

$$A = g(r)\mathbf{e}_r \times \mathbf{u} = g(r)\mathbf{e}_r \times u\mathbf{e}_z = \nabla f(r) \times \mathbf{u} = \nabla \times (f(r)\mathbf{u}), \quad (15)$$

since $\mathbf{e}_r \times \mathbf{e}_z = \mathbf{e}_\phi$. We need to find $f(r)$.

From Eqs. (14) and (13)

$$\mathbf{v} = \mathbf{u} + \nabla \times \mathbf{A} = \mathbf{u} + \nabla \times \nabla \times (f(r)\mathbf{u}), \quad (16)$$

$$\nabla \times \mathbf{v} = \nabla \times \nabla \times \nabla \times (f(r)\mathbf{u}), \quad (17)$$

$$= [\nabla(\nabla \cdot) - \nabla^2] \nabla \times (f(r)\mathbf{u}), \quad (18)$$

$$= -\nabla^2 \nabla \times (f(r)\mathbf{u}), \quad (19)$$

$$\nabla^2 \nabla \times \mathbf{v} = -\nabla^2 \nabla^2 \nabla \times (f(r)\mathbf{u}) = 0, \quad (20)$$

$$= -\nabla^2 \nabla^2 \nabla(f(r) \times \mathbf{u}) = 0, \quad (21)$$

$$\nabla \nabla^2 \nabla^2 f(r) = 0. \quad (22)$$

This evolution uses such things as $\nabla \cdot \nabla \times = 0$, the expansion for **curl curl**, etc. Since f only depends on r $\nabla = \partial/\partial r$ etc. There are 5 derivatives of f in the final formula. We want

to integrate this equation. The first integral is $\nabla^2 \nabla^2 f = \text{constant} = 0$, where the choice $\text{constant} = 0$ comes from hindsight. To go on

$$\nabla^2 \nabla^2 f = \nabla^2 h = 0, \quad \nabla^2 f = h, \quad (23)$$

$$\nabla^2 h = \frac{1}{r^2} \frac{\partial}{\partial r} r^2 \frac{\partial h}{\partial r} = 0, \quad h = \frac{2a}{r}, \quad (24)$$

$$\nabla^2 f = h = \frac{2a}{r}, \quad (25)$$

$$f = ar + \frac{b}{r}, \quad (26)$$

where a and b are constants to be determined. Use $f(r)$ in Eq. (16) and find

$$\mathbf{v} = \mathbf{u} - \frac{a}{r} [\mathbf{u} + \mathbf{e}_r(\mathbf{u} \cdot \mathbf{e}_r)] - \frac{b}{r^3} [\mathbf{u} - 3\mathbf{e}_r(\mathbf{u} \cdot \mathbf{e}_r)]. \quad (27)$$

To find a and b ask that $\mathbf{v} = 0$ on the surface of the sphere. As \mathbf{v} in Eq. (27) is built up from two independent vectors, \mathbf{u} and \mathbf{e}_r , the amplitude of each must vanish at $r = R$. Thus

$$a = \frac{3}{4}R, \quad b = \frac{1}{4}R^3 \quad (28)$$

and

$$\frac{\mathbf{v}}{u} = \left[1 - \frac{3R}{2r} + \frac{R^3}{r^3}\right] \cos\theta \mathbf{e}_r - \left[1 - \frac{3R}{4r} - \frac{R^3}{4r^3}\right] \sin\theta \mathbf{e}_\theta. \quad (29)$$

Before looking at this result let's go on and calculate a few other things of eventual interest.

We find the pressure associated with the flow by going back to Eq. (12). Again some algebra

$$\nabla P = \eta \nabla^2 \mathbf{v} = \eta \nabla^2 \nabla \times \nabla \times (f\mathbf{u}), \quad (30)$$

$$\nabla P = \eta \nabla^2 [\nabla(\nabla \cdot) - \nabla^2](f\mathbf{u}), \quad (31)$$

$$\nabla P = \eta \nabla^2 \nabla(\nabla \cdot)(f\mathbf{u}) = \eta \nabla \nabla^2 (\nabla \cdot f\mathbf{u}), \quad (32)$$

$$P = \eta \nabla^2 (\nabla \cdot f\mathbf{u}), \quad (33)$$

$$P = \eta \nabla^2 (\mathbf{u} \cdot \nabla f) = \eta (\mathbf{u} \cdot \nabla) \nabla^2 f = \eta (\mathbf{u} \cdot \nabla) \frac{3R}{2r}. \quad (34)$$

$$(35)$$

And finally

$$P = -\frac{3\eta u}{2R} (\mathbf{e}_z \cdot \mathbf{e}_r) \frac{R^2}{r^2}. \quad (36)$$

Armed with this expression and the equation for \mathbf{v} one can learn the net force on the sphere.

Again there is much detail See LL (20.13) et. seq. Except for numbers the answer must

scale as P times the area that P works on, i.e., πR^2 . The force is opposite to the direction the sphere is moving

$$\mathbf{F} \propto R^2 \times P(r = R) \approx \eta R u = -6\pi\eta R u \mathbf{e}_u. \quad (37)$$

Summary

$$\frac{\mathbf{v}}{u} = \left[1 - \frac{3R}{2r} + \frac{R^3}{r^3} \right] \cos\theta \mathbf{e}_r - \left[1 - \frac{3R}{4r} - \frac{R^3}{4r^3} \right] \sin\theta \mathbf{e}_\theta, \quad (38)$$

$$P = -\frac{3\eta u}{2R} (\mathbf{e}_z \cdot \mathbf{e}_r) \frac{R^2}{r^2}, \quad (39)$$

$$\mathbf{F} = -6\pi\eta R u \mathbf{e}_u. \quad (40)$$

5. Terminal velocity and such.

A sphere of radius R , density ρ_M , in a viscous liquid and in the presence of gravity obeys the equation of motion

$$M\dot{u} = -6\pi\eta R u \mathbf{e}_u - Mg, \quad (41)$$

where u is the velocity of the sphere and M its mass. Re-arrange this to read

$$\dot{u} = -\frac{1}{\tau_S} u - g, \quad (42)$$

where

$$\frac{1}{\tau_S} = \frac{6\pi\eta R}{M}. \quad (43)$$

Solution to this equation is

$$u(t) = u(0)e^{-\frac{t}{\tau_S}} + g\tau_S(1 - e^{-\frac{t}{\tau_S}}). \quad (44)$$

1. The initial velocity decays away on time scale τ_S .
2. The terminal velocity, $u_T = g\tau_S$ is established on the same time scale.
3. You can read the terminal velocity from Eq. (42) with $\dot{u} = 0$. It is that velocity for which the Stokes drag balances the driving force.

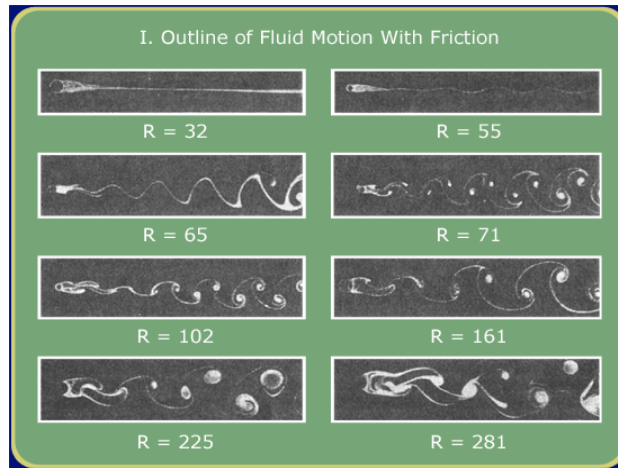


FIG. 4:

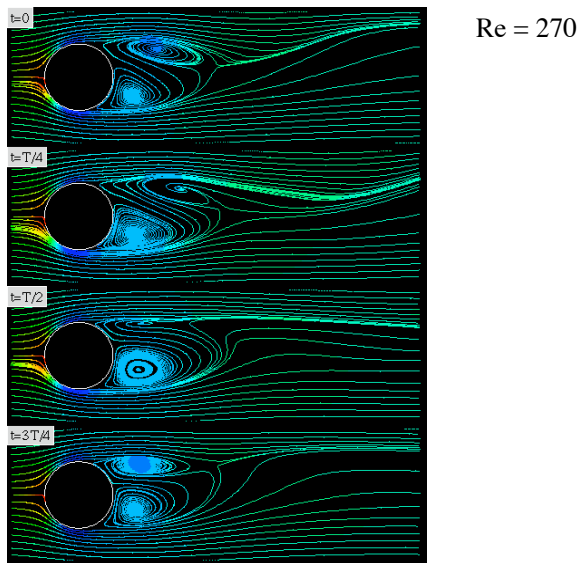


FIG. 5:

6. High Reynolds number.